UNCLASSIFIE

Armed Services Technical Information Agents

ARLINGTON HALL STATION ARLINGTON 12 VIRGINIA

FOR
MICRO-CARD

CONTROL ONLY

NOTICE: WHEN GOVERNMENT OR OTHER DRAWINGS, SPECIFICATIONS OF OF ARE USED FOR ANY PURPOSE OTHER THAN IN CONNECTION WITH A DEFINITE GOVERNMENT PROTUREMENT OPERATION, THE U.S. COVERNMENT THERE IN RESPONSIBILITY, NOR ANY OBLIGATION WHATSOEVER; AND THE FACT THE COVERNMENT MAY HAVE FORMULATED, FURNISHED, OF ME ANY WAY RESPONDED TO BE RESEARCH. THE PROTUCTION OF OTHER DATA IS NOT TO BE RESEARCH. THE PROTUCTION OF OTHER DATA IS NOT TO BE RESEARCH. THE PROTUCTION OF OTHER DATA IS NOT THE DATA IS NO

Best Available Copy LASSIFIED

FILE SORY



AD No. 65 2 6 FRE COPY

PROCESS REPORT NO. 20-339

MOTION OF A TUMBLING RE-ENTRY BODY

E. F. DOBIES

THE PROTESTION LABORATORY
CAUSORMIA INSTITUTE OF TECHNOLOGY
PLEADENA, CAUSORNIA
NOVEMBER 22, 1957

ORDCIT Project
Contract No. DA-04-495-Ord 18
Department of the Army
ORDNANCE CORPS

Progress Report No. 20-339

THE EQUATIONS OF MOTION OF A TUMBLING RE-ENTRY BUDY

E. F. Dobies

A. R. Hibbs, Chief Research Analysis Section

Copy No. A 45

Best Available Copy

JET PROPULSION LABORATORY California Institute of Technology Pasadena, California November 22, 1957

CONTENTS

		Page
1.	Coordinate Systems	1
11.	Trajectory Motion	. 4
III.	Angular Mation	5
IV.	Aerodynamic Forces and Moments	8
٧.	Summary	10
Nom	nenclature	11
	FIGURES	
١.	Space Coordinate System	. 1
2.	Body Coordinate System	. 2
3.	Orientation Angles	. 2

THIS REPORT HAS BEEN DISTRIBUTED ACCORDING TO SECTIONS A, C, AND DA OF THE SUBCOMMITTEE ON ANAF/GM MAILING LIST, OFFICE OF THE ASSISTANT SECRETARY OF DEFENSE (RESEARCH AND DEVSLOPMENT), GUIDED MISSILE TECHNICAL INFORMATION DISTRIBUTION LIST, MMJ. 200/14, LIST NO. 14, DATED 1 JUNE 1957.

ABSTRACT

This Report presents a set of Equations, which may be used to describe the re-entry trajectory of a coasting tumbling rocket. The Equations of motion are kept as general as possible, with the epitons that the azimuth coordinate is linearized, and sand Magnus forces are neglected.

I. COORDINATE SYSTEMS

Fixed at the center of the earth is the origin of an XYZ coordinate system (Fig. 1). The Y axis passes through the point at which the initial conditions are established, the XY plane contains the target, and the Z axis completes a right-hand coordinate system.

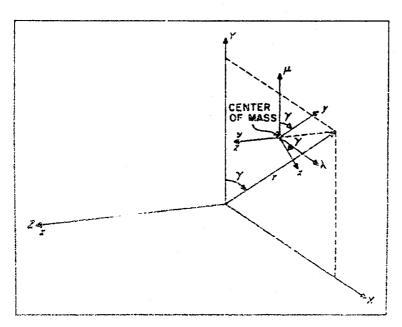


Fig. 1. Space Coordinate System

The rocker center of mass is located by the cylindrical coordinates r, y, z: r is the distance from the origin to the projection of the rocket center of mass on the XY plane, y is the angle between Y and r, and z is identical to Z. There are two sets of space axes located with their origins at the rocket center of mass. The xyz coordinate system is so oriented that the axy plane is parallel to the XYZ axes. The xyz coordinate system is so oriented that the xyy plane is parallel to the XY plane, and y is parallel to r. Also located with its origin at the rocket center of mass is a set of $\xi \eta \zeta$ body axes (Fig. 2). The toll axis is ξ , the yaw axis is η , and the pitch axis is ζ .

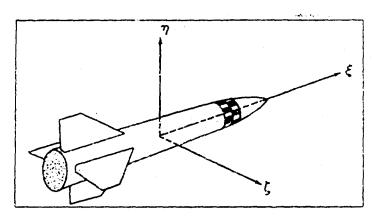


Fig. 2. Body Coordinate System

The orientation of the body with respect to the $\lambda\mu\nu$ coordinate system is described by the Euler angles ϕ , θ , ψ , in the following manner (Fig. 3)¹. Starting with $\xi\eta$ ζ axes respectively coincident with the $\lambda\mu\nu$ axes, the $\xi\eta$ ζ set is rotated counterclockwise by an angle ϕ about the ζ axis. The second rotation is counterclockwise by an angle θ about the ξ axis; whereas, the third rotation is counterclockwise by an angle ψ about the ζ axis. Also, it should be noted that

¹Figure 4-6 from Classical Mechanics by Herbert Goldstein, Copyright 1950 by Addison-Wesley Publishing Company, Inc., Reading, Mass. U.S.A. Permission to use this figure in this report only granted by the copyright owner, Addison-Wesley Publishing Company, Inc.

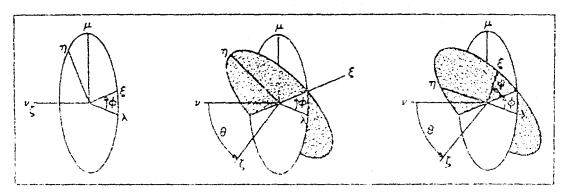


Fig. 3. Orientation Angles

the $\lambda\mu\nu$ coordinate system is obtained by rotating the xyz coordinate system counterclockwise by the angle y about the z axis.

The matrix A (y, ϕ , θ , ψ) is used to transform vectors from xyz coordinates to $\lambda\mu\nu$ coordinates: whereas, its inverse A^{-1} (y, ϕ , θ , ψ) is used to perform the inverse transformation. These matrices are:

$$A = \begin{bmatrix} \cos\psi \cos(\phi + \gamma) - \cos\theta \sin(\phi + \gamma) \sin\psi & \cos\psi \sin(\phi + \gamma) + \cos\theta \cos(\phi + \gamma) \sin\psi & \sin\psi \sin\theta \\ -\sin\psi \cos(\phi + \gamma) - \cos\theta \sin(\phi + \gamma) \cos\psi & -\sin\psi \sin(\phi + \gamma) + \cos\theta \cos(\phi + \gamma) \cos\psi & \cos\psi \sin\theta \end{bmatrix}$$

$$\sin\theta \sin(\phi + \gamma) = -\sin\theta \cos(\phi + \gamma) \cos\theta \cos\theta$$

$$A^{-1} = \begin{bmatrix} \cos\psi \cos(\phi + \gamma) - \cos\theta \sin(\phi + \gamma) \sin\psi & -\sin\psi \cos(\phi + \gamma) - \cos\theta \sin(\phi + \gamma) \cos\psi & \sin\theta \sin(\phi + \gamma) \\ \cos\psi \sin(\phi + \gamma) + \cos\theta \cos(\phi + \gamma) \sin\psi & -\sin\psi \sin(\phi + \gamma) + \cos\theta \cos(\phi + \gamma) \cos\psi & -\sin\theta \cos(\phi + \gamma) \end{bmatrix}$$

$$\sin\psi \sin\theta \qquad \cos\psi \sin\theta \qquad \cos\phi$$

II. TRAJECTORY MOTION

If motion in the z direction is small, the Equations describing the trajectory of the rocket center of mass can be written in the cylindrical coordinates as

$$\frac{d\gamma}{dt} = \frac{v_x}{r}$$

$$\frac{dr}{dt} = v_y$$

$$\frac{dz}{dt} = v_z$$
(1)

$$\frac{dv_x}{dt} = \frac{D}{m} - \frac{v_x v_y}{r}$$

$$\frac{dv_y}{dt} = \frac{L}{m} + \frac{v_x^2}{r} - g_0 \left(\frac{r_0}{r}\right)^2$$

$$\frac{dv_z}{dt} = \frac{S}{m}$$
(2)

where

 $v_x = \text{component of velocity vector along } x \text{ axis}$

vy = component of velocity vector along y axis

 v_z = component of velocity vector along z axis

D = component of aerodynamic force vector along x axis

L = component of aerodynamic force along y axis

S = component of acrodynamic force along z axis

m = coasting mass of the re-entry body

go = sea-level acceleration of gravity

 r_0 = sea-level radius of the earth

III. ANGULAR MOTION

Euler's Equations are used to describe the angular motion of the body about its center of mass

$$I_{\xi} \frac{d\omega_{\xi}}{dt} - \omega_{\eta} \omega_{\zeta} (I_{\eta} - I_{\zeta}) = M_{\xi}$$

$$I_{\eta} \frac{d\omega_{\eta}}{dt} - \omega_{\zeta} \omega_{\xi} (I_{\zeta} - I_{\xi}) = M_{\eta}$$

$$I_{\xi} \frac{d\omega_{\zeta}}{dt} - \omega_{\xi} \omega_{\eta} (I_{\xi} - I_{\eta}) = M_{\zeta}$$
(3)

where

 l_4 = principal margent of inertia about the ith axia

 $\omega_I = \text{component}$ of angular velocity vector along the ith axis

M. - moment along the ith axis

In order to obtain the Equations of motion in terms of Euler angles, new compensate for the angular velocity vector are defined.

$$\frac{d\phi}{dt} = \omega_{\phi}$$

$$\frac{d\hat{v}}{dt} = \omega_{\theta}$$

$$\frac{d\hat{\psi}}{dt} = \omega_{\psi}$$

$$\frac{d\psi}{dt} = \omega_{\psi}$$

In the body system of coordinates, we has the components

$$(\omega_{\phi})_{\xi} = \omega_{\phi} \sin \theta \sin \psi$$
 $(\omega_{\phi})_{\eta} = \omega_{\phi} \sin \theta \cos \psi$ $(\omega_{\phi})_{\gamma} = \omega_{\phi} \cos \theta$

 ω_{θ} has t'e components

$$(\omega_{\theta})_{\xi} = \omega_{\theta} \cos \psi$$
 $(\omega_{\theta})_{\eta} = -\omega_{\theta} \sin \psi$ $(\omega_{\theta})_{\zeta} = 0$

and whas the components

$$(\omega_{\psi})_{\xi} = 0$$
 $(\omega_{\psi})_{\eta} = 0$ $(\omega_{\psi})_{\zeta} = \omega_{\psi}$

Adding these components, the components of the angular velocity vector in body coordinates are as follows:

$$\omega_{\xi} = \omega_{\phi} \sin \theta \sin \psi + \omega_{\theta} \cos \psi$$

$$\omega_{\eta} = \omega_{\phi} \sin \theta \cos \psi + \omega_{\phi} \sin \psi$$

$$\omega_{\zeta} = \omega_{\phi} \cos \theta + \omega_{\psi}$$
(5)

After taking time derivations, it follows that

$$\frac{d\omega_{\phi}}{dt} = \frac{d\omega_{\xi}}{dt} - \frac{d\omega_{\eta}}{dt} - \omega_{\theta}(\omega_{\phi} \cos\theta - \omega_{\psi})$$

$$\frac{d\omega_{\theta}}{dt} = \cos\psi \frac{d\omega_{\xi}}{dt} - \sin\psi \frac{d\omega_{\eta}}{dt} - \omega_{\phi} \omega_{\psi} \sin\theta$$

$$\frac{d\omega_{\psi}}{dt} = \frac{d\omega_{\zeta}}{dt} - \frac{d}{dt} \left[\omega_{\phi} \cos\theta\right]$$
(6)

Combining Eqs. (3) with Eqs. (6) gives

$$\sin\theta \frac{d\omega_{\phi}}{dt} = \frac{\sin\psi}{I_{\xi}} \left[M_{\xi} + (I_{\eta} - I_{\xi}) \omega_{\eta} \omega_{\xi} \right] + \frac{\cos\psi}{I_{\eta}} \left[M_{\eta} + (I_{\zeta} - I_{\xi}) \omega_{\zeta} \omega_{\xi} \right] - \omega_{\theta}(\omega_{\phi} \cos\theta - \omega_{\psi})$$

$$\frac{d\omega_{\theta}}{dt} = \frac{\cos\psi}{I_{\xi}} \left[M_{\xi} + (I_{\eta} - I_{\xi}) \omega_{\eta} \omega_{\zeta} \right] - \frac{\sin\psi}{I_{\eta}} \left[M_{\eta} + (I_{\zeta} - I_{\xi}) \omega_{\zeta} \omega_{\xi} \right] - \omega_{\phi} \omega_{\psi} \sin\theta$$

$$\frac{d\omega_{\zeta}}{dt} = \frac{1}{I_{\zeta}} \left[M_{\zeta} + (I_{\xi} - I_{\eta}) \omega_{\xi} \omega_{\eta} \right] - \frac{d}{dt} \left[\omega_{\phi} \cos\theta \right]$$
(7)

The rotational motion can be completely described by Eqs. (4), (5) and (7).

IV. AERODYNAMIC FORCES AND MOMENTS

Aerodynamic force and moment coefficients are usually available in body coordinates; therefore, it is necessary to find the components of the stream velocity vector in body coordinates

$$\begin{vmatrix} u_{\zeta} \\ u_{\eta} \\ u_{\zeta} \end{vmatrix} = A \begin{vmatrix} -(v_{x} - w_{x}) \\ -v_{y} \\ -(v_{z} - w_{z}) \end{vmatrix}$$
(8)

$$u_{\xi} = -(v_{x} - w_{x})[\cos\psi \cos(\phi + \gamma) - \cos\theta \sin(\phi + \gamma) \sin\psi]$$

$$-v_{y}[\cos\psi \sin(\phi + \gamma) + \cos\theta \cos(\phi + \gamma) \sin\psi] - (v_{z} - w_{z}) \sin\psi \sin\theta$$

$$u_{\eta} = (v_{x} - w_{x})[\sin\psi \cos(\phi + \gamma) + \cos\theta \sin(\phi + \gamma) \cos\psi]$$

$$+v_{y}[\sin\psi \sin(\phi + \gamma) - \cos\theta \cos(\phi + \gamma) \cos\psi] - (v_{z} - w_{z}) \cos\psi \sin\theta$$

$$u_{\zeta} = -(v_{x} - w_{x}) \sin\theta \sin(\phi + \gamma) + v_{y} \sin\theta \cos(\phi + \gamma) - (v_{z} - w_{z}) \cos\theta$$

in body coordinates, the aerodynamic forces are then found from

$$F_{i} = \frac{u_{i}}{\left|u_{i}\right|} \frac{1}{2} \rho(r) \left[u_{\xi}^{2} + u_{\eta}^{2} + u_{\zeta}^{2}\right] d^{2} C_{i}(\alpha, \beta, \delta, M, Re) \qquad i = \xi, \eta, \zeta$$
 (10)

where

$$\alpha$$
 = angle of attack

$$\beta = \text{roll angle}$$

$$\delta$$
 = fin deflection

Equations (2) require accodynamic force components in space coordinates; therefore $F_{\mathcal{E}}$, F_{π} , and F_{ζ} must be transformed to space coordinates

,多了 養 成 義立 化液理性 1.17、1.00以下,我们就是我们就是一个一个人的,我们也不会会会

$$\begin{vmatrix}
D \\
L \\
S
\end{vmatrix} = A^{-1} \begin{vmatrix}
F_{\xi} \\
F_{\eta}
\end{vmatrix}$$
(11)

Since the aerodynamic coefficients are functions of angle of attack and roll angle, it is necessary to determine these angles.

$$D = F_{\xi} \left[\cos \psi \cos(\phi + \gamma) - \cos \theta \sin(\phi + \gamma) \sin \psi \right] - F_{\eta}$$

$$\left[\sin \psi \cos(\phi + \gamma) + \cos \theta \sin(\phi + \gamma) \cos \psi \right] + F_{\zeta} \sin \theta \sin(\phi + \gamma)$$

$$L = F_{\xi} \left[\cos \psi \sin(\phi + \gamma) + \cos \theta \cos(\phi + \gamma) \sin \psi \right] - F_{\eta}$$

$$\left[\sin \psi \sin(\phi + \gamma) - \cos \theta \cos(\phi + \gamma) \cos \psi \right] - F_{\zeta} \sin \theta \cos(\phi + \gamma)$$

$$S = F_{\xi} \sin \theta \sin \psi + F_{\eta} \sin \theta \cos \psi + F_{\zeta} \cos \theta$$

$$(12)$$

$$\cos \alpha = \frac{-u_{\xi}}{\left(u_{\xi}^{2} + u_{\eta}^{2} + u_{\zeta}^{2}\right)^{\frac{1}{2}}} \qquad \cos \beta = \frac{-u_{\eta}}{\left(u_{\eta}^{2} + u_{\zeta}^{2}\right)^{\frac{1}{2}}}$$
(13)

The pitching moment is given by

$$M_{\zeta} = \frac{-u_{\eta}}{\left|u_{\tau}\right|} \frac{1}{2} \rho \left(u_{\xi}^{2} + u_{\eta}^{2} + u_{\zeta}^{2}\right) d^{3} C_{M\zeta} (\alpha, \beta, \delta, M, Re)$$
 (14)

the yawing moment by

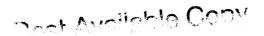
$$M_{\eta} = \frac{u_{\zeta}}{\left|u_{\zeta}\right|} \frac{1}{2} \rho \left(u_{\zeta}^{2} + u_{\eta}^{2} + u_{\zeta}^{2}\right) d^{3} C_{M\eta} \left(\alpha, \beta, \delta, M, Re\right)$$
 (15)

and the rolling moment by

$$M_{\xi} = \frac{1}{2} \rho \left(u_{\xi}^2 + u_{\eta}^2 + u_{\zeta}^2 \right) d^2 l C_{M\xi} (\alpha, \beta, \delta, M, Re)$$
 (16)

V. SUMMARY

The trajectory Equations (1 and 2) simultaneously with the rotation Equations (4, 5, and 7) describe the dynamics of the coasting rocket. The aerodynamic forces are given by Eqs. (10) and (12), whereas, the aerodynamic moments are obtained from Eqs. (14), (15), and (16). The forces and moments are functions of angle of attack, roll angle, and fin deflection. Angle of attack and roll angle are computed by Eq. (13); whereas, fin deflection is a programmed input. All aerodynamic coefficients must be supplied as inputs.



NOMENCLATURE

 $A(y, \phi, \psi) = \text{transformation matrix from } xyz \text{ axes } \xi \eta \zeta \text{ axes.}$

 $A^{-1}(\gamma, \phi, \theta, \psi)$ = transformation matrix from $\xi \eta \zeta$ axes to xyz axes.

 C_{ζ} = aerodynamic coefficient of normal force in yaw plane.

 C_{η} = aerodynamic coefficient of normal force in pitch plane.

 $C_{\mathcal{E}}$ = aerodynamic coefficient of cord force.

 $C_{M\zeta}$ = aerodynamic coefficient of pitch about center of mass.

 $C_{M\eta}$ = aerodynamic coefficient of yaw about certer of mass.

 $C_{M\xi}$ = aerodynamic coefficient of roll about center of mass.

d - rocket base diameter.

D = aerodynamic force component along x axis.

 F_{ζ} = aerodynamic normal force in yaw plane.

 F_{π} = aerodynamic normal force in pitch plane.

 $F_{\mathcal{E}}$ = aerodynamic cord force.

 g_0 = sea-level acceleration of gravity.

 I_{χ} = pitch moment of inertia.

 I_{η} = yaw moment of inertia.

 $I_{\mathcal{E}}$ = roll moment of inertia.

l = distance between missile axis and fin center of pressure.

L = aerodynamic force component along y axis.

m =mass of coasting rocket.

M = Mach number.

 M_{χ} = pitch moment, see Eq. (14).

 $M_{\eta} = \text{yaw moment, see Eq. (15).}$

 $M_{\mathcal{E}} = \text{roll moment, see Eq. (16)}.$

 r_0 = sea-level radius of earth.

NOMENCLATURE (Cont'd)

Rc = Reynolds number.

r, y, z = carth-fixed secondary coordinate system (Fig. 1).

S = aerodynamic force component along z axis.

 $u_{\mathcal{E}}$, u_{η} , $u_{\mathcal{L}}$ = components of stream velocity in body coordinates.

 v_x = center of mass velocity vector component along x axis.

 v_y = center of mass velocity vector component along y axis.

 v_z = center of mass velocity vector component along z axis.

 $w_x = \text{downrange wind velocity.}$

 $w_x =$ crossrange wind velocity.

x, y, z = local space coordinates associated with r, y, z (Fig. 1).

X, Y, Z = earth-fixed primary coordinate system (Fig. 1).

 α = angle of attack: angle between stream velocity vector and ξ axis.

 β = roll angle: angle between plane of angle of attack and η axis.

 δ = fin deflection.

 λ , μ , ν = local space coordinates associated with X, Y, Z (Figs. 1 and 3).

 ξ , η , ζ = body-fixed coordinate system (Fig. 2).

 $\rho(r) = atmospheric density.$

 ϕ , θ , ψ = Euler orientation angles (Fig. 3).

 ω_{ξ} = pitch rate.

 $\omega_n = yaw rute.$

 $\omega_{\mathcal{E}}$ = roll rate.

 ω_{ϕ} , ω_{θ} , ω_{ψ} = see Eq. (4).